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(54) **Brazing copper end rings and bars in an induction motor rotor by induction heating**

(57) An induction motor rotor is manufactured by assembling copper end ring laminations 30, 35 on each axial end of a core assembly 15 with slots 20, 34 aligned and copper rotor bars 40 in the slots and induction braz-

ing the ends of the copper bars to the copper end ring laminations. The forming of the end rings by laminations greatly reduces machining and scrap; and the use of induction heating reduces exposure of the core assembly to the high heat of brazing.

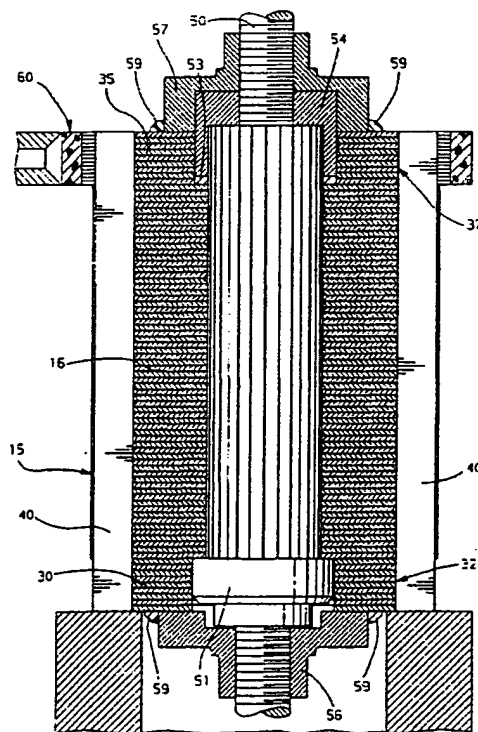


FIG. 2

Description

Background of the Invention

The technical field of this invention is the manufacture of induction motor rotors having copper end rings and copper bars.

Induction motor rotors are often manufactured with a plurality of straight, electrically conducting bars equally spaced from and extending parallel to the rotor axis around the rotor core assembly. At each axial end, these bars are joined to an electrically conducting end ring to form a "squirrel cage" rotor. During manufacture of the rotor, the bars must be physically and electrically joined to the end rings so as to provide both physical strength and a low resistance electrical current path. Even a small resistance can produce a significant voltage drop with the large currents produced in such a rotor. Copper is a favored material for such bars and rings, due to its low resistance and reasonable cost.

The joining of copper bars and end rings for induction motor rotors is known to be accomplished by a brazing process in which the parts to be joined are fluxed and flame heated to the braze temperature, at which the braze material is applied to the joint area. Flame heating may take from 5 to 15 minutes per rotor end; and it is hard to obtain even heating of the copper even with the use of multiple flame devices.

In another known method of joining copper bars and end rings for induction motor rotors, a preformed piece of solder material is inserted into the joint area, with the parts separately fluxed or the flux included in the solder material. The parts are then heated in a furnace to the braze temperature, at which the braze material flows into the joint area. This process provides more even heating but may take from 0.5 to 2 hours to reach the proper temperature.

In each of these methods, the rotor laminations are subjected to temperatures of 650 to 760 degrees C for extended periods of time. This can lead to core losses in the lamination steel, which produces motor inefficiency. These types of heating methods can also limit the type of brazing material used, since some brazing material will only melt above the Curie Temperature of the lamination steel.

Summary of the Invention

The object of this invention is to provide a method of joining the ends of copper bars to copper end rings in the manufacture of induction motor rotors which is fast and produces a minimal negative effect on the remainder of the rotor. This object is realized by induction brazing the ends of the copper bars to the copper end rings. In this process, the end rings are clamped tightly on each axial end of the core assembly with the rotor bars retained in the core slots and extending through the end ring slots. At each end, an induction coil is placed coax-

ially around the copper end ring and relative axial rotation is provided between the end ring and the induction coil while a high frequency alternating current is generated in the induction coil to braze the copper bars to the copper end rings by electromagnetically induced heat. Induction heating provides heat more efficiently to the region to be brazed with less waste heat to the remainder of the assembly than with prior art heating methods using flame or ovens. This produces time savings for reduced costs in the manufacturing process and reduces the possibility of reduced motor efficiency due to overheating of the core.

A method for brazing copper end rings and bars in an induction motor rotor by induction heating in accordance with the present invention is characterised by the features specified in Claim 1.

Brief Description of the Drawings

The present invention will now be described, by way of example, with reference to the accompanying drawings, in which:

FIG. 1 shows a step in the method of manufacturing an induction motor rotor according to the invention; FIG. 2 shows another step in the method of manufacturing an induction motor rotor according to the invention;

FIG. 3 shows a completed induction motor rotor manufactured according to the invention;

FIG. 4 shows a perspective view of an end ring lamination in the rotor of FIG. 3;

FIG. 5 shows an enlarged axial view of a portion of the end ring lamination of FIG. 4;

FIG. 6 shows a perspective view of a core lamination in the rotor of FIG. 3; and

FIG. 7 shows an enlarged axial view of a portion of the core lamination of FIG. 6.

Description of a Preferred Embodiment

Referring to FIG. 3, an induction motor rotor 10 is built on a steel shaft 12 having an interior splined portion 14. Dimensions given in the following description are approximate dimensions of one possible embodiment and are not critical unless specifically stated. A ferromagnetic core 15 comprises a plurality of core laminations 16, which are axially stacked and spline fitted to interior splined portion 14 of shaft 12 in the normal manner. FIG. 6 shows a typical core lamination 16, which is annular in shape with spline teeth 18 at its inner diameter (43 mm) to fit corresponding splines of shaft 12 and a plurality (68, for example) of equally spaced, radially aligned slots 20 opening to outer diameter 19 (126 mm). These and all other dimensions and numbers given herein are approximate and for example only, unless otherwise stated. FIG. 7 shows a close-up of a slot 20, which is partially closed at its radially outer end by circumferen-

tial extensions 22 of the lamination material for rotor bar retention. Slot 20 measures 1.4 mm wide at its radially inner end, which is 15 mm from the outer diameter, and 2.6 mm wide adjacent extensions 22; the latter measuring 0.5 mm radially and leaving an opening of 0.8 mm.

At one axial end of the core 15, a plurality of end ring laminations 30, stamped from sheet copper, are brazed together to form a slotted copper end ring 32. FIG. 4 shows an end ring lamination 30 in perspective view. End ring lamination 30 is 2.3 mm in width and annular in shape, with an unsplined inner diameter (52 mm) and a plurality of radially aligned slots 34 opening to its outer diameter 36 (125 mm). A similar end ring 37 comprising end ring laminations 35 is shown in FIG. 1 at the opposite axial end of core 15. Slots 34 of end ring lamination 30, as well as similar slots of end ring laminations 35, are equal in number, aligned with, and of essentially the shape and size as core laminations 16, but without the circumferential extensions of core lamination 16, so that they measure only 14 mm in from the 125 mm outer diameter of the lamination.

Referring again to FIG. 3, a plurality of rotor bars 40 extend axially through the slots of core 15 and end rings 32 and 37. Bars 40 are slightly trapezoidal in cross section, with a slight increase in width in the radial direction to fit the cross section of slots 20 of FIG. 7 and slots 34 of FIG. 5. Bars 40 are uniform in cross section along their axial length and are physically and electrically joined to each of end rings 32 and 37 by brazing or a similar process to form a shorted turn rotor conductor structure locked onto core 15 of rotor 10. A containment cup 42 covers the axial end of rotor 10 which comprises end ring 32; and a similar containment cup 44 covers the opposite axial end of rotor 10, which comprises end ring 37.

Essentially, the structure of rotor 10 is the same as that of the prior art except for laminations 30 of end ring 32 and laminations 35 of end ring 37. These laminations enable the end rings to be formed by the stamping of laminations from sheet copper, orienting and stacking the laminations, and joining the laminations to bars 40 by brazing or a similar process. Although a small amount of machining may be done to smooth the end rings for a precise fit of the containment cups 42 and 44, the major machining required for end rings of the prior art is eliminated for significant time and cost savings in manufacture. Additional cost savings result from the reduction in scrap produced. Moreover, with proper joining such as by copper to copper brazing, the laminated structure of the end rings does not introduce significant resistance into the rotor current paths; and tests show equivalent performance by motors having rotors made according to this invention.

In manufacture, core laminations 16 are stamped from sheet steel and stacked in the normal manner on a brazing arbor 50 with the slots and splines of all laminations aligned. Brazing arbor 50, shown in FIG. 1, includes a containment ring 51 at one end which is just

large enough in diameter to retain the core laminations. Although shown as a separate part threaded onto arbor 50, containment ring 51 may be an integral part of the arbor. A washer 53 and lam containment ring 54 at the other end are also just large enough in diameter to retain the core laminations, which are tightly retained in a stack when lam containment ring 54 is threaded on arbor 50. Copper rotor bars 40 are then inserted in the slots of the stacked core so that they project from each axial end.

End ring laminations 30 and 35 are stamped from sheet copper on a punch press, and a predetermined number (e.g. 8 or 9) are assembled at each end of the core laminations by inserting axially onto the projecting ends of rotor bars 40. The end ring laminations have a larger inner diameter than the outer diameter of containment ring 51; washer 52 and lam containment ring 54, which axially retain the core laminations, so they can be pushed past these tool pieces against the core laminations. End ring containment caps 56 and 57 are then threaded onto the ends of the arbor to hold the end ring laminations tightly in place. The core and end ring laminations, which are held tightly together on brazing arbor 50 to prevent undesirable expansion during the brazing process, form a lamination assembly 58 with rotor bars 40 inserted.

Lamination assembly 58 is next placed in a rotation fixture. With all laminations aligned and held tightly together, the rotor bars 40 are then pushed axially partly out of the assembly, at least by the axial width of an end ring, so that they project outward from the other end of the assembly by an equal amount. The end ring laminations and rotor bars are now ready for fluxing, as shown in FIG. 1. A solder dam material 59 is applied around the circumference of end ring containment caps 56 and 57 where they abut the outermost end ring laminations in order to prevent flux from migrating under these caps during the brazing process. A high temperature flux is applied to the projecting rotor bars at one axial end and the exposed slots of the end ring laminations at the other axial end of rotor 10, such as by spraying from a squeeze bottle 58, while rotating rotor 10 on the fixture. Rotor bars 40 are then pushed back into lamination assembly 58 so that their ends are flush with the outermost one of end ring laminations 30 and 35 at each end; and the flux is thus distributed across the surfaces between the ends of bars 40 and end ring laminations 30 and 35. Additional flux is then applied as required to the outer surfaces of the region to be brazed, such as the edges of end ring laminations 30 and 35 and the surface where rotor bars 40 intersect end ring laminations 30 and 35.

The assembly is now fluxed and ready for brazing. As seen in FIG. 2, an induction coil 60, which may, for example be the output element of an Elva Minac (R) electrical induction heating unit, is placed around and coaxial with the copper end ring laminations 30 at one axial end of the lamination stack. During brazing, the unit supplies induction coil 60 with alternating current at a high frequency of 12 KHz; and this current induces cur-

rents in the copper end ring laminations 30 and 35 and the ends of copper bars 40 within the coil. The heat produced by these induced currents raises the temperature of the region to be brazed to the brazing temperature to join the copper end ring laminations and rotor bars 40 together physically, to form a strong physical conductor structure on the rotor core, and electrically, to create low resistance current paths between bars 40 through end ring laminations 30 and 35. The unit described is capable of being programmed for two consecutive periods so that a higher power may be provided for a first period to raise the temperature to the brazing temperature and the power may be then automatically reduced to hold the brazing temperature for an additional period. During the brazing process, the lamination assembly is rotated at 5-10 RPM within induction coil 60 to distribute the heat evenly throughout the brazing region. Induction heating by coil 60 as described provides heat more efficiently to the region to be brazed with less waste heat to the remainder of the assembly than with prior art heating methods using flame or ovens. This produces time savings for reduced costs in the manufacturing process and reduces the possibility of reduced motor efficiency due to overheating of the core. When the brazing process at one end of the rotor is completed, the process is repeated at the other end.

The result of the previous processes is the transformation of lamination assembly 58 into a core and conductor subassembly 65 of an induction motor rotor. The various containment pieces are removed, and subassembly 65 is removed from the brazing arbor. It is installed in a fixture, and the rotor shaft 12 is installed. Next, some machining of the copper end rings is performed. The assembly is rotated on a lathe and copper is removed to meet the required runout of copper end rings 32 and 37 for the fit of containment cups 42 and 44. Containment cups 42 and 44 are then heated by an induction or other heating unit and installed over copper end rings 32 and 37, the cups shrinking to a tight fit as they cool. Finally, the rotor core is varnish impregnated and buffed to remove excess varnish from the surface, with the result being rotor 10 of FIG. 3.

Claims

1. A method of making an induction motor rotor 10 comprising the steps:

assembling a plurality of core laminations 16 into a core assembly 15 having radially oriented and axially extending slots 20;
assembling the core assembly with a pair of copper end rings 32, 37 and a plurality of copper bars 40 in a tool 50, 51, 53, 54, 56, 57 to form a lamination assembly 58, the copper end rings being disposed at opposite axial ends of the core assembly with each having a plurality

of slots 34 similar to and aligned with those of the core assembly to continue the same axially, one of the plurality of copper bars being retained in each of the slots of the core assembly and extending through the aligned slots of the copper end rings;

applying flux to adjacent surfaces of the copper end rings and copper bars;

placing an induction coil 60 coaxially around each of the copper end rings and providing relative axial rotation between the lamination assembly and the induction coil while generating a high frequency alternating current within the induction coil to braze the copper bars to the copper end rings by induction heat; and removing the lamination assembly from the tool and assembling it on a rotor shaft 12.

2. A method of making an induction motor rotor 10 comprising the steps:

assembling a plurality of core laminations 16 into a core assembly 15 having radially oriented and axially extending slots 20;

stamping a plurality of end ring laminations 30, 35 from a sheet of electrically conducting material, each of the copper end ring laminations having a plurality of radially oriented slots 34;

assembling the core assembly, the plurality of end ring laminations and a plurality of electrically conducting rotor bars 40 in a tool 50, 51, 53, 54, 56, 57 to form a lamination assembly 58 with a first number of the plurality of electrically conducting end ring laminations 30 forming a first end ring lamination stack 32 at one axial end of the core assembly, a second number of the plurality of end ring laminations 35 forming a second end ring lamination stack 37 at the other end of the core assembly, the slots of the first and second end ring lamination stacks being aligned with those of the core assembly to continue the same axially, and one of the plurality of electrically conducting rotor bars retained in each of the slots of the core assembly and extending through each of the first and second end ring lamination stacks;

applying flux to adjacent surfaces of the copper end rings and copper bars;

placing an induction coil 60 coaxially around each of the copper end rings and providing relative axial rotation between the end rings and the induction coil while generating a high frequency alternating current within the induction coil to braze the copper bars to the copper end rings by induction heat; and removing the lamination assembly from the tool and assembling it on a rotor shaft 12.

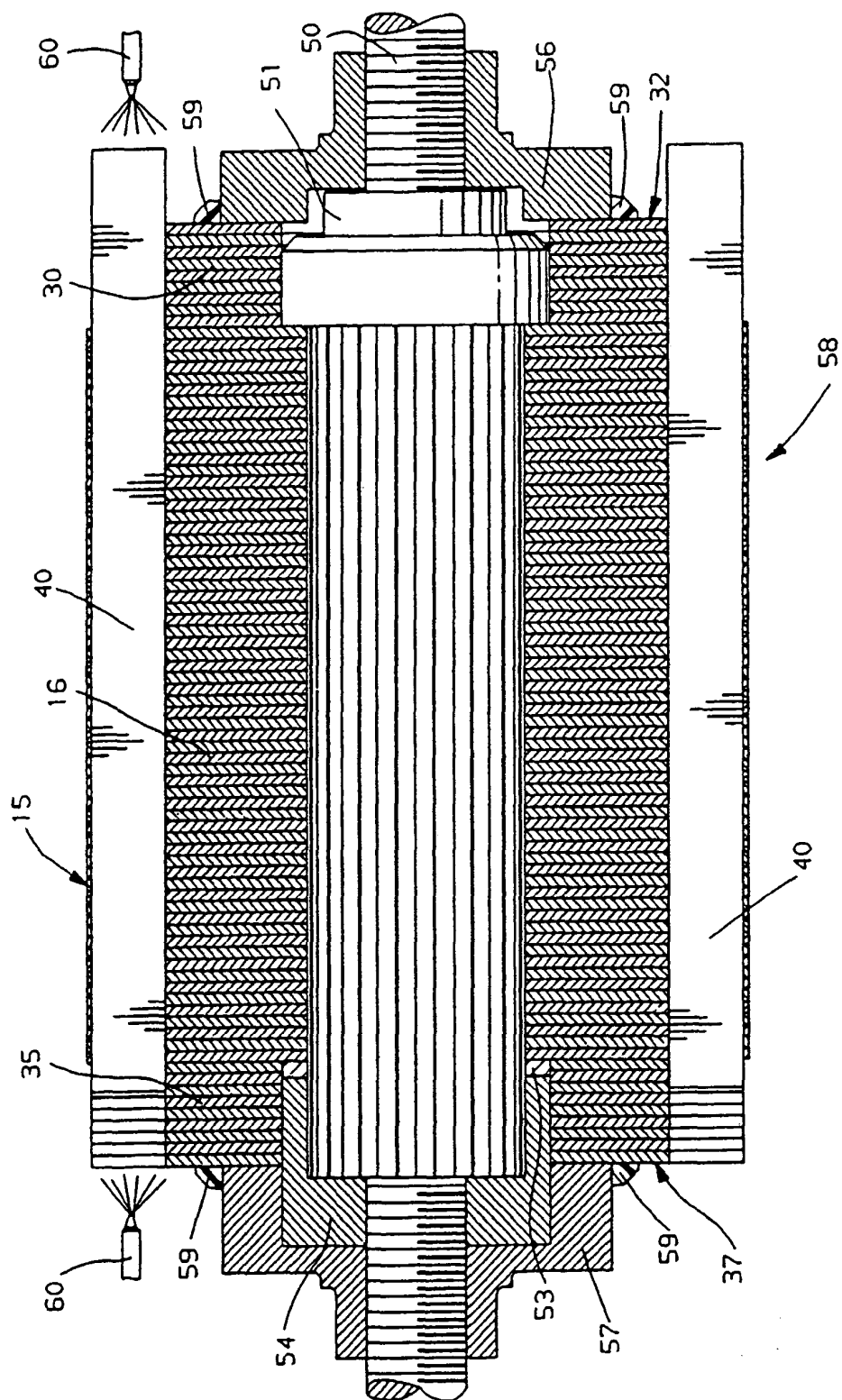


FIG. 1

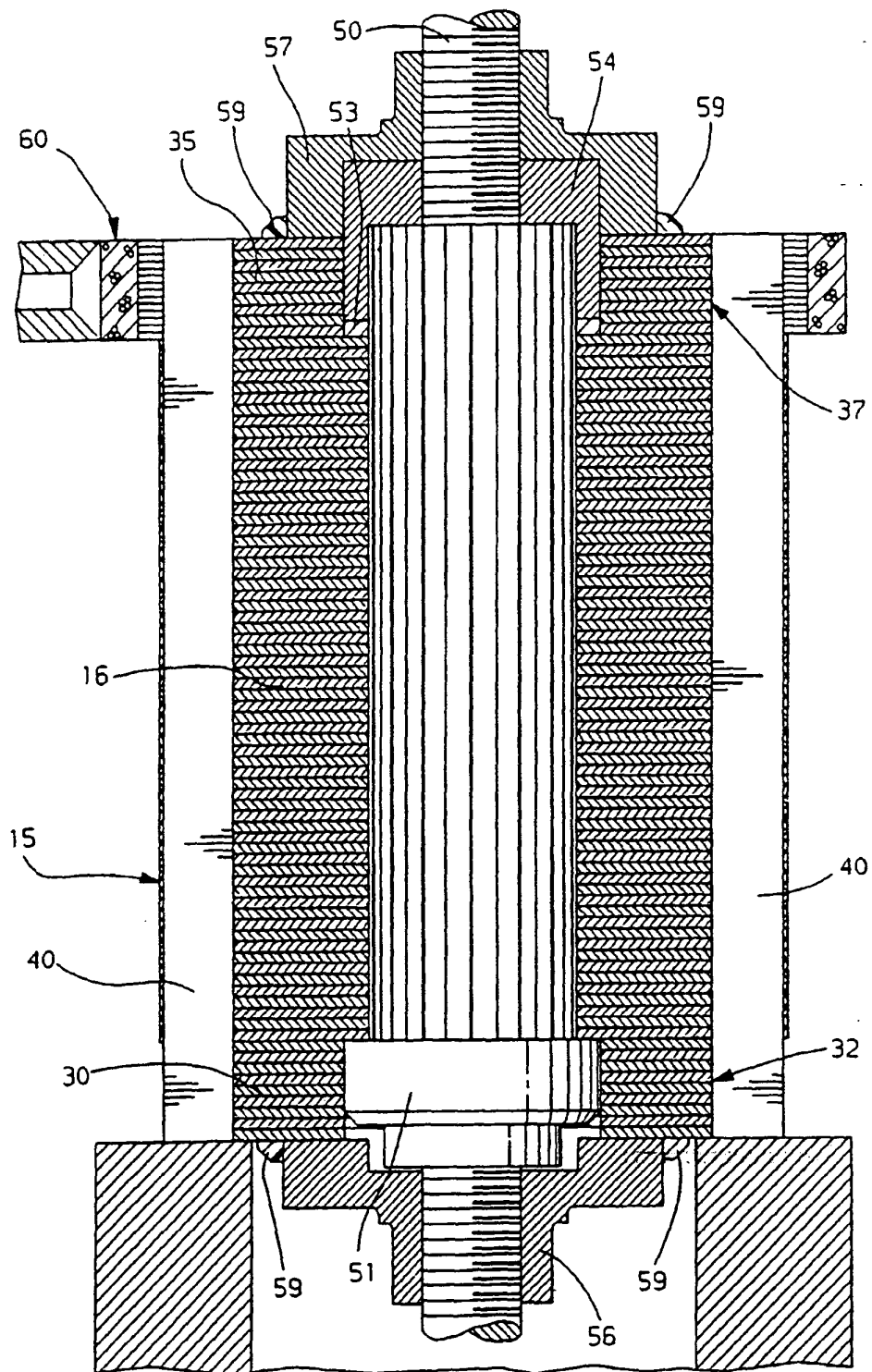


FIG. 2

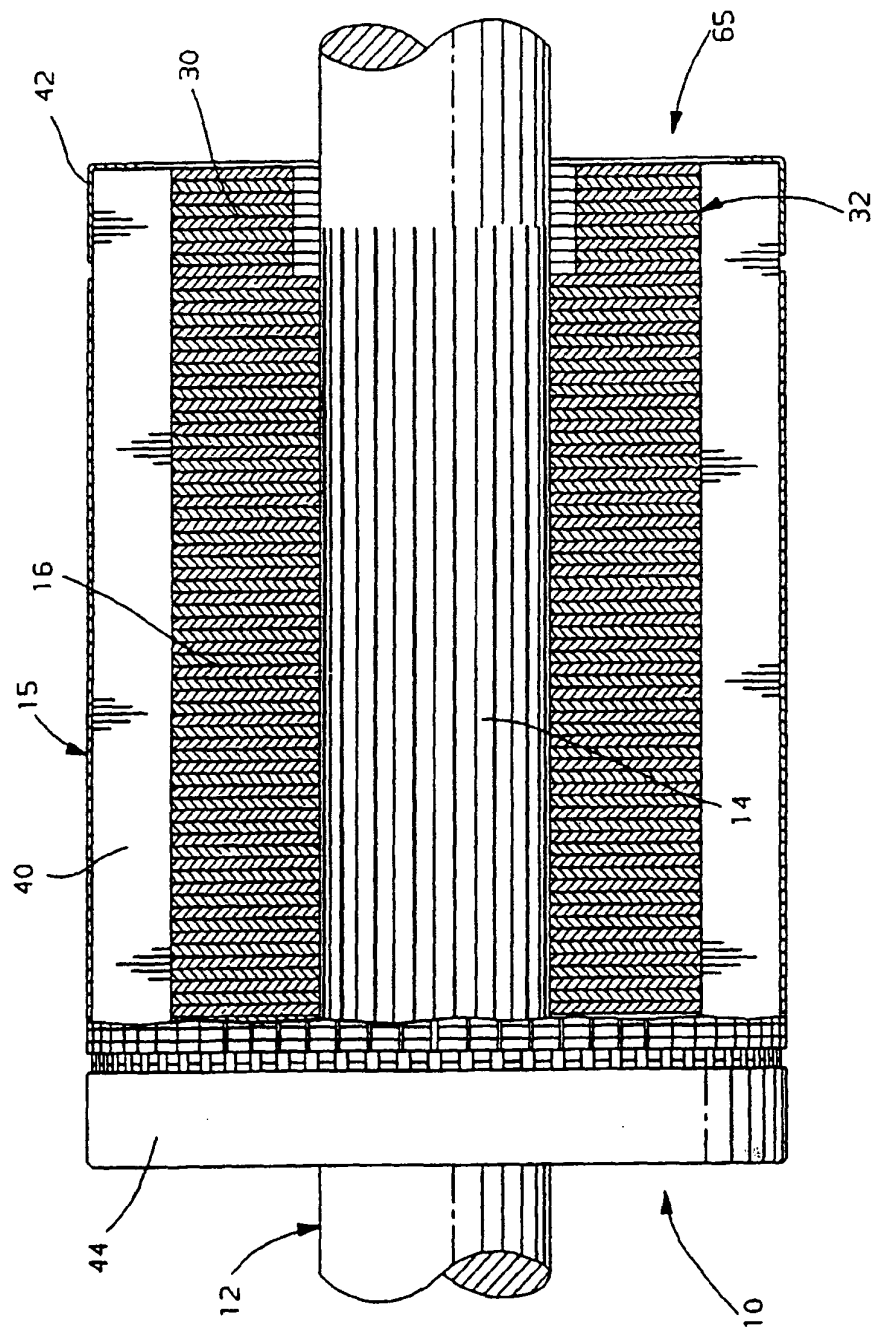


FIG. 3

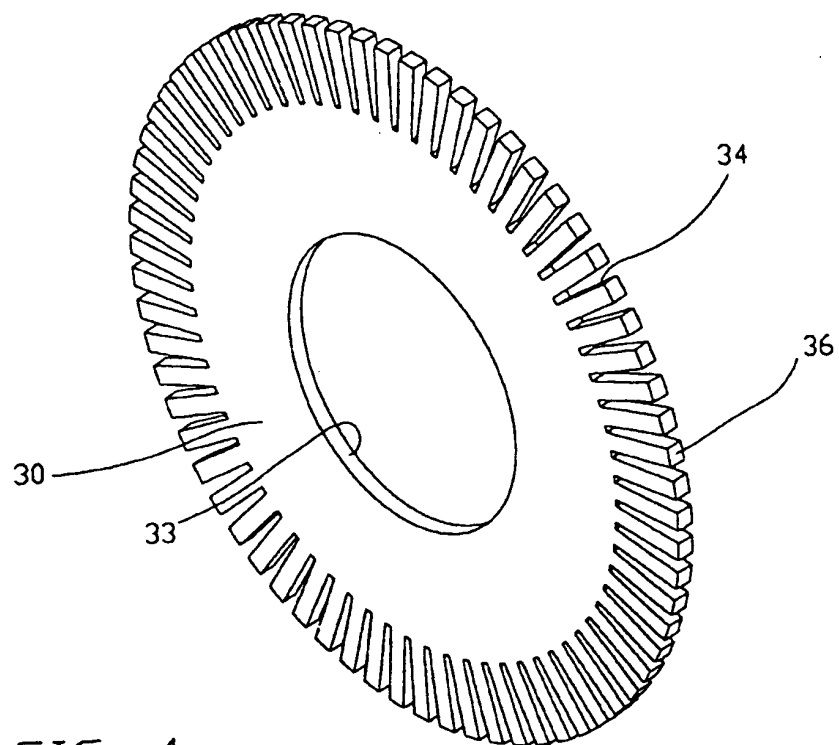


FIG. 4

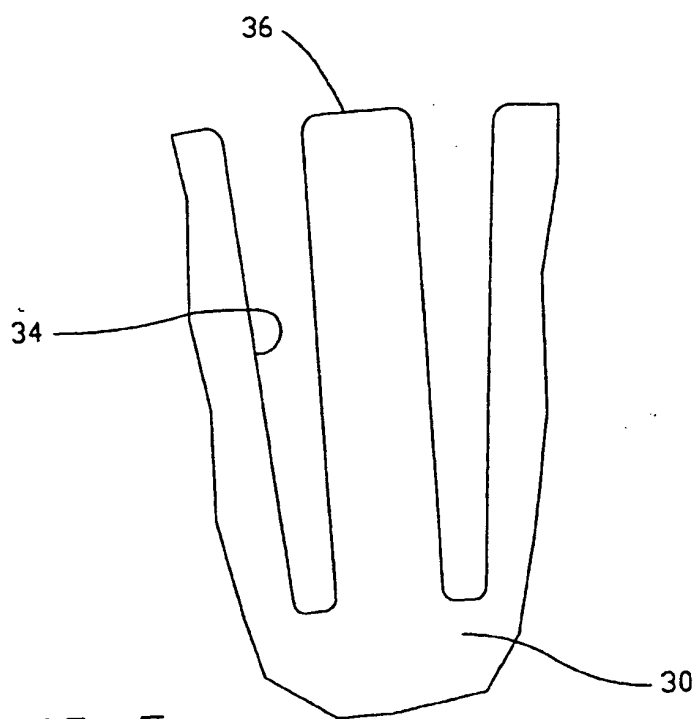


FIG. 5

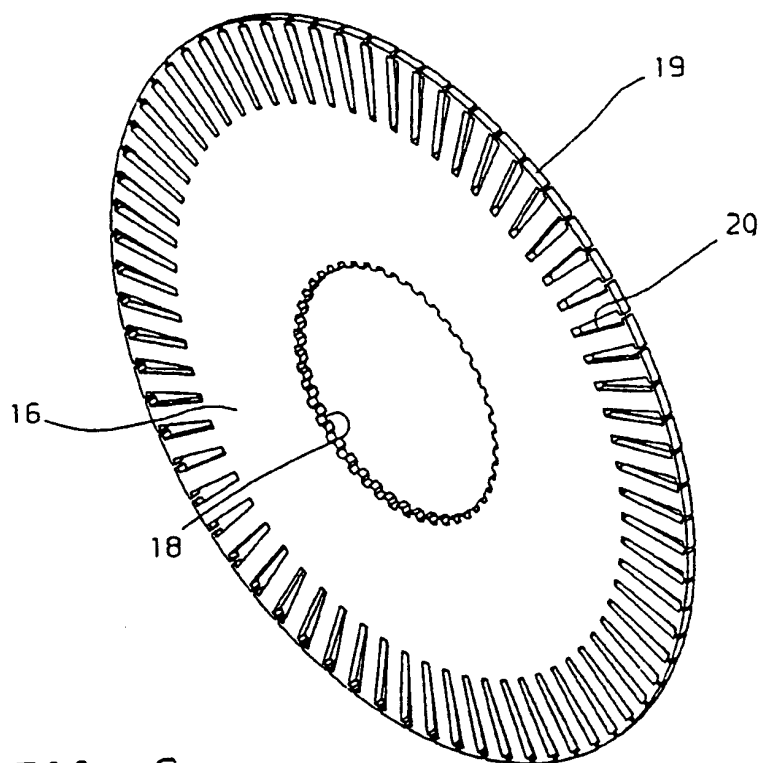


FIG. 6

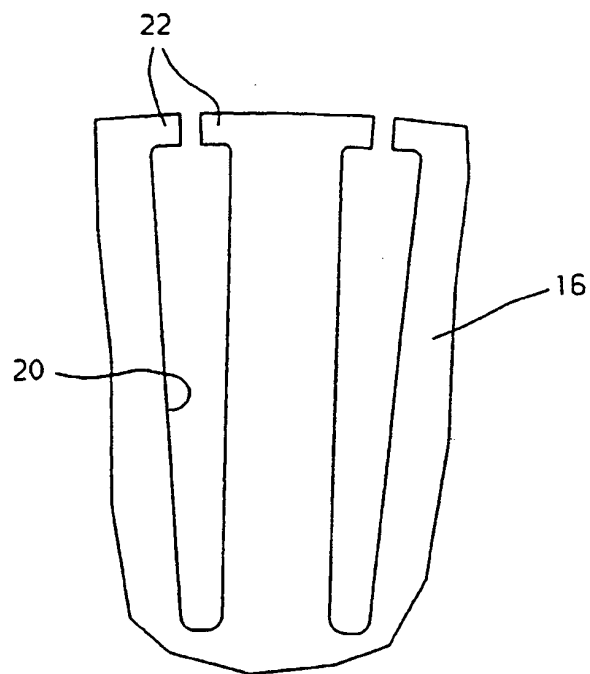


FIG. 7



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(54) **Brazing copper end rings and bars in an induction motor rotor by induction heating**

(57) An induction motor rotor is manufactured by assembling copper end ring laminations 30, 35 on each axial end of a core assembly 15 with slots 20, 34 aligned and copper rotor bars 40 in the slots and induction brazing the ends of the copper bars to the copper end ring laminations. The forming of the end rings by laminations greatly reduces machining and scrap; and the use of induction heating reduces exposure of the core assembly to the high heat of brazing.

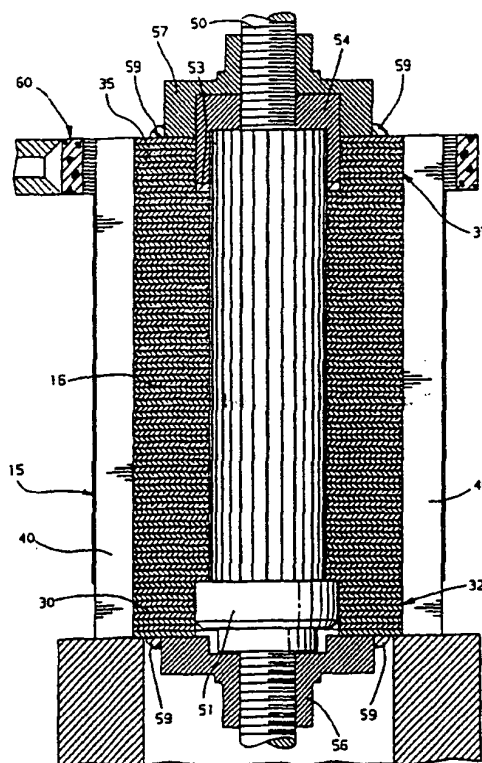


FIG. 2



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number

DOCUMENTS CONSIDERED TO BE RELEVANT			EP 96201188.8
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 6)
X	US 4249098 A (KARLEN et al.) 03 February 1981 (03.02.81), column 6, line 11 - column 7, line 14.	1	H 02 K 17/16 H 02 K 15/02 B 23 K 1/002
A	---	2	
A	US 3705971 A (LINOS, J.J.) 12 December 1972 (12.12.72), the whole document.	1,2	
A	US 2286008 A (PFALZGRAFF, R.M.) 02 August 1940 (02.08.40), the whole document.	1,2	
			TECHNICAL FIELDS SEARCHED (Int. Cl. 6)
			H 02 K B 23 K
The present search report has been drawn up for all claims			
Place of search VIENNA		Date of completion of the search 30-11-1998	Examiner HAWEL
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons A : member of the same patent family, corresponding document	
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			

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